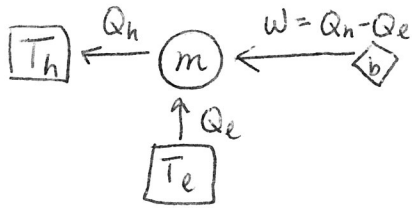


1. Heat Pump. (a) Show that for a reversible heat pump the energy required per unit of heat delivered inside the building is given by the Carnot efficiency  $\frac{W}{Q_h} = \eta_c = \frac{T_h - T_c}{T_h}$



Reversible  $\therefore \Delta S_{TOT} = 0$

$$S_h + S_e + S_m + S_b = 0 \quad S_m = 0 \quad S_b = 0$$

$$\frac{Q_h}{T_h} - \frac{Q_e}{T_e} = 0 \Rightarrow \frac{T_e}{T_h} = \frac{Q_e}{Q_h}$$

$$\frac{W}{Q_h} = \frac{Q_h - Q_e}{Q_h} = 1 - \frac{Q_e}{Q_h} = 1 - \frac{T_e}{T_h} = \frac{T_h - T_e}{T_h} = \frac{kT_h - kT_e}{kT_h} = \frac{T_h - T_e}{T_h}$$

What happens if the heat pump is not reversible?  $\Delta S_{TOT} > 0$

$$\frac{Q_h}{T_h} - \frac{Q_e}{T_e} > 0 \Rightarrow \frac{Q_e}{Q_h} < \frac{T_e}{T_h} \Rightarrow \frac{Q_e}{Q_h} = 1 - \frac{W}{Q_h} < \frac{T_e}{T_h} \Rightarrow \frac{W}{Q_h} > 1 - \frac{T_e}{T_h}$$

more energy is required per unit of heat delivered inside the building

$$\frac{W}{Q_h} > \frac{T_h - T_e}{T_h}$$

(b) Assume that the electricity consumed by a reversible heat pump must itself be generated by a Carnot engine operating between  $T_{hh}$  and  $T_c$ . What is the ratio  $Q_{hh}/Q_h$  of the heat consumed at  $T_{hh}$  to the heat delivered at  $T_h$ ?

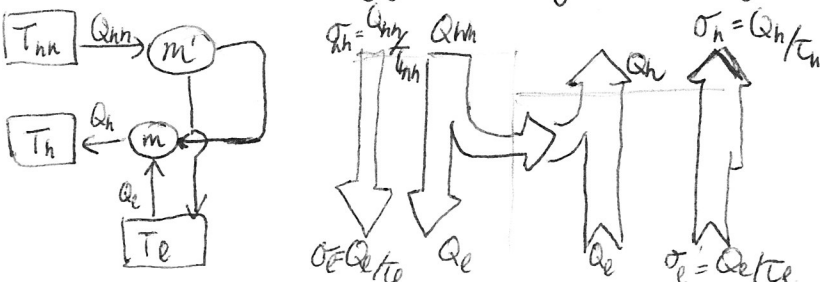
$$\left(\frac{W}{Q_{hh}}\right)_{rev} = \frac{T_{hh} - T_e}{T_{hh}} \quad \left(\frac{W}{Q_h}\right)_{rev} = \frac{T_h - T_e}{T_h}$$

$$\frac{Q_{hh}}{Q_h} = \frac{\left(\frac{W}{Q_{hh}}\right)_{rev}}{\left(\frac{W}{Q_h}\right)_{rev}} = \frac{\left(\frac{T_{hh} - T_e}{T_{hh}}\right)}{\left(\frac{T_h - T_e}{T_h}\right)} = \frac{T_{hh} (T_h - T_e)}{T_h (T_{hh} - T_e)}$$

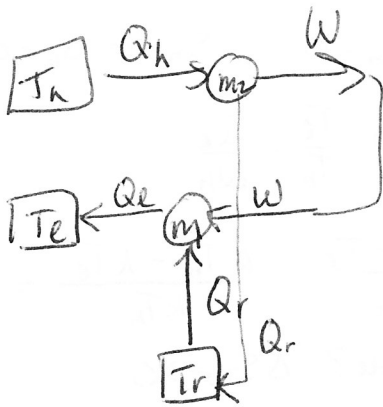
Give numerical values for  $T_{hh} = 600K$ ,  $T_h = 300K$ ,  $T_e = 270K$ .

$$\frac{Q_{hh}}{Q_h} = \frac{600(300 - 270)}{300(600 - 270)} = \frac{2 \cdot 30}{330} = 0.1818$$

(c) Draw an energy-entropy flow diagram



# 4. Heat Engine



X 0

(b) Assume that the efficiency of the engine is  $\eta$ . The work done by the engine is  $W$ . The heat rejected to the cold reservoir is  $Q_c$ . The heat taken from the hot reservoir is  $Q_h$ . The heat taken from the cold reservoir is  $Q_c$ . The work done by the engine is  $W$ . The heat rejected to the cold reservoir is  $Q_c$ . The heat taken from the hot reservoir is  $Q_h$ . The heat taken from the cold reservoir is  $Q_c$ .

$$\eta = \frac{W}{Q_h} = \frac{Q_h - Q_c}{Q_h} = 1 - \frac{Q_c}{Q_h}$$

$$\frac{Q_c}{Q_h} = 1 - \eta$$

$$\frac{Q_c}{Q_h} = \frac{T_c}{T_h}$$

$$1 - \eta = \frac{T_c}{T_h}$$

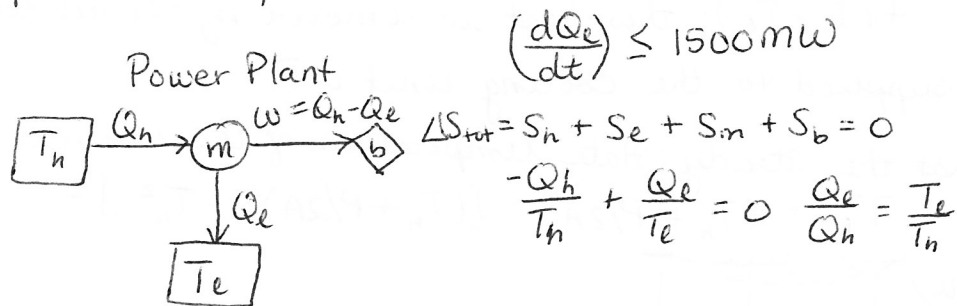
$$\eta = 1 - \frac{T_c}{T_h}$$

The numerical value for  $T_h$  is 300K,  $T_c$  is 200K.

$$\eta = 1 - \frac{200}{300} = 1 - \frac{2}{3} = \frac{1}{3} = 0.333$$



5. Thermal Pollution. A river with a water temperature  $T_e = 20^\circ\text{C} = 293\text{K}$  is to be used as the low temperature reservoir of a large power plant, with a steam temperature of  $T_h = 500^\circ\text{C} = 773\text{K}$ . If ecological considerations limit the amount of heat that can be dumped into the river to 1500 MW, what is the largest electrical output that the plant can deliver?



$$W = Q_h - Q_e$$

$$\frac{dW}{dt} = \frac{dQ_h}{dt} - \frac{dQ_e}{dt} = \frac{T_h}{T_e} \frac{dQ_e}{dt} - \frac{dQ_e}{dt} = \frac{dQ_e}{dt} \left( \frac{T_h}{T_e} - 1 \right)$$

$$\frac{dW}{dt} \leq (1500 \text{ MW}) \left[ \frac{773}{293} - 1 \right] = 2747 \text{ MW}$$

If improvements in hot-steam technology would permit raising  $T_h$  by  $100^\circ\text{C}$ , what effect would this have on the plant capacity?

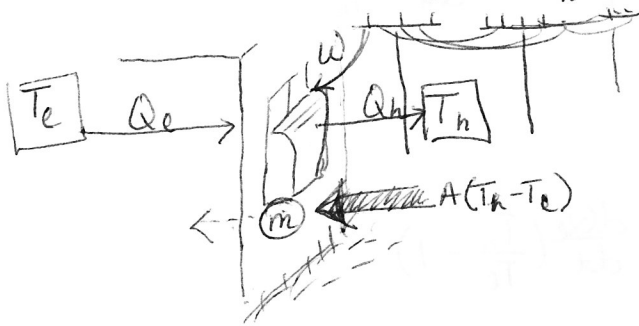
$$\frac{dW}{dt} \leq (1500 \text{ MW}) \left[ \frac{873}{293} - 1 \right] = 2969 \text{ MW} \quad \text{increase production}$$

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6. Room Air Conditioner. A room air conditioner operates as a Carnot cycle refrigerator between an outside temperature  $T_h$  and a room at a lower temperature  $T_e$ . The room gains heat from the outdoors at a rate  $A(T_h - T_e)$ ; this heat is removed by the air conditioner. The power supplied to the cooling unit is  $P$ .

(a) Show that the steady-state temperature of the room is

$$T_e = (T_h + P/2A) - [(T_h + P/2A)^2 - T_h^2]^{1/2}$$



$$\frac{dQ_e}{dt} = A(T_h - T_e) \quad \frac{dW}{dt} = P$$

$$Q_e + W = Q_h = \frac{T_h}{T_e} Q_e$$

$$W = Q_e \left( \frac{T_h}{T_e} - 1 \right)$$

$$\frac{dW}{dt} = \frac{dQ_e}{dt} \left( \frac{T_h}{T_e} - 1 \right)$$

$$P = A(T_h - T_e) \left( \frac{T_h}{T_e} - 1 \right)$$

$$(P/A) T_e = (T_h - T_e)(T_h - T_e)$$

$$T_h^2 - 2T_e T_h + T_e^2 - (P/A) T_e = 0$$

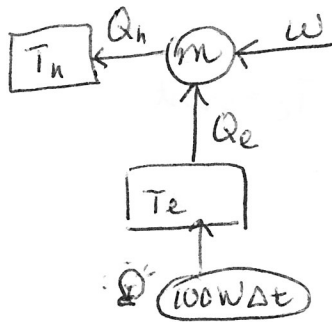
$$T_e^2 + T_e(-P/A - 2T_h) + T_h^2 = 0$$

$$T_e = \frac{(P/A + 2T_h) \pm \sqrt{(P/A - 2T_h)^2 - 4T_h^2}}{2} = (T_h + P/2A) - \sqrt{(T_h + P/2A)^2 - T_h^2}$$

(b) If the outdoors is at  $37^\circ\text{C}$  ( $\approx 307\text{K}$ ) and the room is maintained at  $17^\circ\text{C}$  by a cooling power of  $2\text{kW}$ , find the heat loss coef  $A$  of the room in  $\text{W K}^{-1}$ .  $T_h = 307\text{K}$   $T_e = 287\text{K}$   $P = 2000\text{W}$

$$A = \frac{P T_e}{(T_h - T_e)^2} = \frac{(2000\text{W}) 287\text{K}}{(307 - 287)^2 \text{K}^2} = 1435 \text{W K}^{-1}$$

## 7. Light Bulb in a Refrigerator.



$$W = Q_h - Q_c$$

$$\Delta S_{TOT} \geq 0$$

$$\frac{Q_h}{T_h} + \frac{(100W\Delta t - Q_c)}{T_c} \geq 0$$

$$P \frac{dW}{dt} = P \left[ \frac{dQ_h}{dt} - \frac{dQ_c}{dt} \right]$$

$$Q_h \geq \frac{T_h}{T_c} [Q_c - 100W\Delta t]$$

$$\frac{dQ_h}{dt} = P \left[ \frac{dQ_c}{dt} - 100W \right]$$

$$\frac{dQ_h}{dt} \geq \frac{T_h}{T_c} \left[ \frac{dQ_c}{dt} - 100W \right]$$

$$P + \frac{dQ_c}{dt} \geq \frac{T_h}{T_c} \left[ \frac{dQ_c}{dt} - 100W \right] \quad P = 100W$$

$$\gamma_c = \left( \frac{Q_c}{W} \right) = \frac{T_c}{T_h - T_c} \quad \text{for a refrigerator } P = 100W$$

$$\frac{dQ_c}{dt} = \left( \frac{T_c}{T_h - T_c} \right) \frac{dW}{dt} = \left( \frac{T_c}{T_h - T_c} \right) P = \left( \frac{T_c}{T_h - T_c} \right) 100$$

$$100 \left[ 1 + \frac{T_c}{T_h - T_c} \right] \geq \frac{T_h}{T_c} \left[ \left( \frac{T_c}{T_h - T_c} \right) 100 + 100 \right]$$

$$\therefore T_c \geq T_h$$

So, no, it can't have  $T_c < T_h$

## 8. Geothermal Energy

$$dQ_h = -mc dT_h$$

$$dE = dQ + dW \quad T_h = T_i \text{ to } T_h = T_f \quad T_c = \text{const}$$

$$dW = -mc dT_h$$

$$W = -mc(T_f - T_i)$$

$$c = 1 \text{ J g}^{-1} \text{ K}^{-1}$$

$$T_i = 600^\circ\text{C}$$

$$W = Q_h - Q_c = -mc(T_f - T_i) - Q_c$$

$$-mc \ln \frac{T_f}{T_i} = \frac{Q_c}{T_c}$$

$$W = -mc(T_f - T_i) + T_c c m \ln \frac{T_f}{T_i}$$

$$c = 1 \text{ J g}^{-1} \text{ K}^{-1} \quad T_i = 873 \text{ K}$$

$$T_f = 383 \text{ K}$$

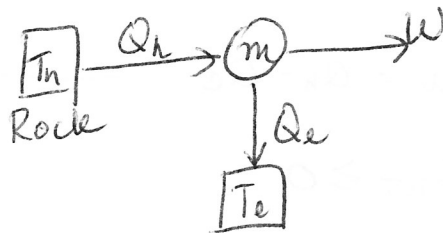
$$T_c = 293 \text{ K}$$

$$m = 10^{14} \text{ kg}$$

$$W = +(10^{14})(1)(8490) + (293)(10^{14})(1) \ln \left( \frac{383}{873} \right)$$

$$W = (618.5 \cdot 10^{14} \text{ J}) \left( \frac{\text{W}}{\text{s}} \right) \frac{10^4 \text{ kW}}{\text{W}} \left( \frac{3600 \text{ s}}{\text{h}} \right) = 6.9 \cdot 10^{12} \frac{\text{kW}}{\text{h}}$$

6.9



$$W = Q_h - Q_c$$

$$\frac{Q_h}{T_h} = \frac{Q_c}{T_c}$$

$$\int \frac{dQ_h}{T_h} = \int -\frac{mc dT_h}{T_h}$$

$$\begin{cases} S_h = -mc \ln \frac{T_f}{T_i} \\ S_c = \frac{Q_c}{T_c} \end{cases}$$

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